



Prime Consulting Engineers Pty. Ltd.

Design Report:

12m Dome Structure (enclosed)

For



Ref: R-22-211-1

Date: 12/05/2022

Amendment: A

Prepared by: KZ

Checked by: SD

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1 Introduction and Scope:

The report and certification are the sole property of Prime Consulting Engineers Pty. Ltd.

Prime Consulting Engineers have been engaged by Extreme Marquees Pty. Ltd. to carry out a structural analysis of 12m dome structure for wind loads region A (non-cyclonic) and snow loads for sub-alpine regions. It should be noted that the outcome of our analysis is limited to the selected items as outlined in this report.

This report shall be read in conjunction with the documents listed in the references (Section 1.2)

1.1 Project Description

The report examines the effect of 3s gust wind of **(refer to summary)** and snow loads of sub-alpine region positioned for the worst effect on the 12m dome structure. The result of this report is also applicable to the smaller dome structure with identical member sizes. The relevant Australian Standards AS1170.0:2002 General principles, AS1170.1:2002 Permanent, imposed and other actions, AS1170.2:2021 Wind actions and AS1170.3 Snow actions are used. The design check is in accordance with AS4100:1998 steel structures.

1.2 References

- The documents referred to in this report are as follows:
 - Report of results produced through SAP2000 V24 software & excel spreadsheets.
 - Detail drawing provided by manufacturer. Refer to appendix 'A'.
- The basic standards used in this report are as follows:
 - AS 1170.0:2002 – Structural Design Actions (Part 0: General principles)
 - AS 1170.1:2002 – Structural Design Actions (Part 1: Permanent, imposed, and other actions)
 - AS 1170.2:2021 – Structural Design Actions (Part 2: Wind Actions)
 - AS 1170.3:2003 – Snow and ice actions.
 - AS4100:1998 – Steel Structures.
- Section Properties of Steel (Q235) Section provided by the client.
- The program(s) used for this analysis are as follows:
 - SAP2000 V24
 - Microsoft Excel

1.3 Notation

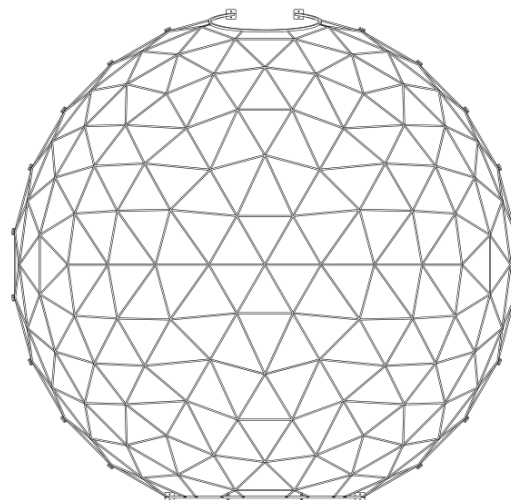
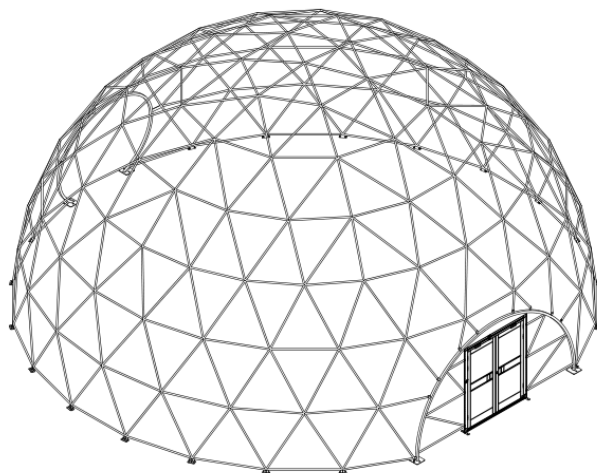
AS/NZS	Australian Standard/New Zealand Standard
FEM/FEA	Finite Element Method/Finite Element Analysis

SLS Serviceability Limit State

ULS Ultimate Limit State

2 Design Overview

2.1 Geometry Data



EXTREME MARQUEES



DOMES RANGE

4m / 5m / 6m / 7m / 8m / 9m / 10m / 11m / 12m

EVENT TENT



ITEM	SPECIFICATION								
Size	4m	5m	6m	7m	8m	9m	10m	11m	12m
Ceiling Height	2.4m	2.5m	3m	3.5m	4m	4.5m	5m	5.5m	6m
Door Size	1200mm W x 1800mm H			1500mm W x 2100mm H			1500mm W x 2400mm H		
Dome Style	Lapela								
Floor Space	12.5 sq.m	17.8 sq.m	28 sq.m	38 sq.m	50 sq.m	63 sq.m	78 sq.m	95 sq.m	113 sq.m
Stand up Capacity	15	24	34	46	60	76	94	114	136
Sit down Capacity	10	16	23	31	40	51	63	76	90
Frame Material	Steel								

Isometric view of structures

2.2 Assumptions & Limitations

- The erected structure is for temporary use only.
- For forecast winds in excess of **(refer to summary)** the dome structure should be completely dismantled.
- The structure may only be used in regions with wind and snow classifications no greater than the limits specified in cl. 5 & 6 of this report.
- Parameters used for wind & snow calculations:
 - TC 2
 - Wind Region A
 - Sub-alpine region (Orange, NSW)
- Topographical factors such as erecting the structure on the crest of a hill or on the top of an escarpment may result in a higher wind speed classification. Thus, special considerations should be taken to the topographical location of the installation site.
- Shall the site conditions, wind or snow parameters exceed prescribed design actions (refer to cl.7), Prime Consulting Engineers Pty. Ltd. should be informed to determine appropriate wind/snow classifications and amend computations accordingly.
- It is assumed that the structure is fully enclosed with equally permeable side walls to calculate Wind Internal Forces.

2.3 Exclusions

- Design of fabric
- Wind actions due to tropical or severe tropical cyclonic areas.
- Snow actions due to snow loads other than Orange, NSW.
- Super imposed loads such as live load.

2.4 Design Parameters and Inputs

2.4.1 Load Cases

1.	G	Permanent actions (Dead load)
3.	Wu	Ultimate wind action (ULS)
4.	Ws	Serviceability wind action (SLS)
5.	S	Snow action (SLS)

2.4.2 Load Combinations

Strength (ULS):

1. 1.35G Permanent action only
3. 0.9G+W_u Permanent and wind actions
4. 1.2G+W_u Permanent and wind actions
5. 1.2G+S Permanent and snow actions

Serviceability (SLS):

2. G+W_s Wind service actions

3 Specifications

3.1 Material Properties

Material Properties 03a - Steel Data								
Material	F _y	F _u	EffF _y	EffF _u	S _{Hard}	S _{Max}	S _{Rup}	FinalSlope
Text	KN/m ²	KN/m ²	KN/m ²	KN/m ²	Unitless	Unitless	Unitless	Unitless
Q235	235000	390000	260000	430000	0.015	0.11	0.17	-0.1

3.2 Member Sizes & Section Properties

Frame Section Properties 01 - General												
SectionName	t ₃	t ₂	t _f	t _w	Area	TorsConst	I ₃₃	I ₂₂	S ₃₃	S ₂₂	Z ₃₃	Z ₂₂
Text	mm	mm	mm	mm	mm ²	mm ⁴	mm ⁴	mm ⁴	mm ³	mm ³	mm ³	mm ³
32x2 CHS	32			2	188.5	42600	21300	21300	1331.3	1331.3	10.63	10.63
30x2 SHS	30	30	2	2	224	43904	29418.67	29418.67	1961.24	1961.24	2356	2356

4 Design Loads

Self weight	G	self weight
3s 120km/hr gust	W _u	0.751 C _{fig} (kPa)
Sub-alpine snow load	W _s	0.13 - 0.68 (kPa)

5 Wind Analysis

5.1 Ultimate



Project: 12m Dome Structure

Jon no. 22-211-1

Designer: KZ

Date: 4/05/2022

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Name	Symbol	Value	Unit	Notes	Ref.
General					
Importance level		3			Table 3.1 - Table 3.2 (AS1170.0)
Annual probability of exceedance		Temporary			Table 3.3
Regional gust wind speed		140.00	Km/hr		
Regional gust wind speed	V_R	38.89	m/s		
Wind Direction Multipliers	M_d	1			Table 3.2 (AS1170.2)
Terrain Category	TC	2			
Terrain Category Multiplier	$M_{Z,Cat}$	0.91			
Shield Multiplier	M_S	1			4.3 (AS1170.2)
Topographic Multiplier	M_t	1			4.4 (AS1170.2)
Site Wind Speed	$V_{Site,\beta}$	35.39	m/s	$V_{Site,\beta} = V_R * M_d * M_{Z,Cat} * M_S * M_t$	
Pitch	α	0	Deg		
Pitch	α	0.000	rad		
Width	B	12	m		
Width Span	S_w	-	m		
Length	D	12	m		
Height	Z	3	m		
Bay Span		-	m		
	h/d	0.25			
	h/b	0.25			
Wind Pressure					
ρ_{air}	ρ	1.2	Kg/m ³		

dynamic response factor	C_{dyn}	1			
Wind Pressure	$\rho * C_{fig}$	0.751	Kg/m ²	$\rho = 0.5 \rho_{air} * (V_{des,\beta})^2 * C_{fig} * C_{dyn}$	2.4 (AS1170.2)
WIND DIRECTION 1 (Perpendicular to Length)					
Internal Pressure					
Opening Assumption	Without Dominant Opening				
Internal Pressure Coefficient (Without Dominant) MIN		-0.3		$C_{pi} = N * C_{pe}$	
Internal Pressure Coefficient (Without Dominant) MAX		0.2			
Internal Pressure Coefficient (With Dominant) MIN					
Internal Pressure Coefficient (With Dominant) MAX					
N					
Combination Factor	$K_{C,i}$	1			
Internal Pressure Coefficient MIN	$C_{p,i}$	-0.30			
Internal Pressure Coefficient MAX	$C_{p,i}$	0.20			
External Pressure					
1. Windward Wall					
External Pressure Coefficient	$C_{P,e}$	0.7			Table 5.4
Area Reduction Factor	K_a	1			
combination factor applied to internal pressures	$K_{C,e}$	0.8			
local pressure factor	K_l	1			
porous cladding reduction factor	K_p	1			
aerodynamic shape factor	$C_{fig,e}$	0.56			
Wind Wall Pressure	P	0.42	kPa		
2. Leeward Wall					
External Pressure Coefficient	$C_{P,e}$	-0.5			Table 5.4
Area Reduction Factor	K_a	1			
combination factor applied to internal pressures	$K_{C,e}$	0.8			
local pressure factor	K_l	1			
porous cladding reduction factor	K_p	1			
aerodynamic shape factor	$C_{fig,e}$	-0.4			

Leeward Wall Pressure	P	-0.30	kPa		
3. Side Wall					
Area Reduction Factor	K _a	1			Table 5.4
combination factor applied to internal pressures	K _{C,e}	0.8			
local pressure factor	K _l	1			
porous cladding reduction factor	K _p	1			
External Pressure Coefficient	C _{P,e}	-0.65		0 to 1h	
External Pressure Coefficient	C _{P,e}	-0.5		1h to 2h	
External Pressure Coefficient	C _{P,e}	-0.3		2h to 3h	
External Pressure Coefficient	C _{P,e}	-0.2		>3h	
aerodynamic shape factor	C _{fig,e}	-0.52		0 to 1h	
aerodynamic shape factor	C _{fig,e}	-0.4		1h to 2h	
aerodynamic shape factor	C _{fig,e}	-0.24		2h to 3h	
aerodynamic shape factor	C _{fig,e}	-0.16		>3h	
Side Wall Pressure	P	-0.39	kPa	0 to 1h	
Side Wall Pressure	P	-0.30	kPa	1h to 2h	
Side Wall Pressure	P	-0.18	kPa	2h to 3h	
Side Wall Pressure	P	-0.12	kPa	>3h	
4. Roof					
r (rise)	r	6	m		
h/r	h/r	0.50			
Breadth Effect		1.00		(b/d) ^{0.25} >1	
Rise-to-span ratio	r/d	0.50			
4.1 Roof Windward Quarter					
U	U	3	m		Table C3
Area Reduction Factor	K _a	1			
combination factor applied to internal pressures	K _{C,e}	0.8			
local pressure factor	K _l	1			
porous cladding reduction factor	K _p	1			
External Pressure Coefficient	C _{P,e}	0.3			
Factored External Pressure Coefficient	C _{P,e}	0.30			
aerodynamic shape factor	C _{fig,e}	0.24			
Pressure	P	0.18	kPa		
4.2 Roof Centre Half					
T	T	6	m		Table C3

Area Reduction Factor	K_a	1		
combination factor applied to internal pressures	$K_{C,e}$	0.8		
local pressure factor	K_l	1		
porous cladding reduction factor	K_p	1		
External Pressure Coefficient	$C_{P,e}$	-0.65		
Factored External Pressure Coefficient	$C_{P,e}$	-0.65		
aerodynamic shape factor	$C_{fig,e}$	-0.52		
Pressure	P	-0.39	kPa	
4.2 Roof Centre Half				
D	D	3	m	Table C3
Area Reduction Factor	K_a	1		
combination factor applied to internal pressures	$K_{C,e}$	0.8		
local pressure factor	K_l	1		
porous cladding reduction factor	K_p	1		
External Pressure Coefficient	$C_{P,e}$	-0.2		
Factored External Pressure Coefficient	$C_{P,e}$	-0.20		
aerodynamic shape factor	$C_{fig,e}$	-0.16		
Pressure	P	-0.12	kPa	

5.1.1 Summary Forces

WIND EXTERNAL PRESSURE (kPa)				
			Wind Direction	
Windward			0.42	
Leeward			-0.30	
Sidewall	0m - 3m		-0.39	
	3m - 6m		-0.30	
	6m - 9m		-0.18	
	> 9m		-0.12	
Roof				
	Windward Quarter (U)	3m	0.18	
	Centre Half (T)	6m	-0.39	
	Leeward Quarter (D)	3m	-0.12	
Wind Internal Pressure (kPa)				
			-0.23	0.15

6 Snow Load

6.1 Sub-Alpine

$$S = S_g \times C_e \times \mu_i$$

Annual probability of exceedance: 1/20

Snow region: Orange, NSW

$S_g = 0.9 \text{ kPa}$

$$C_e = 1$$

Average slope:

Segment 1: $6^\circ \rightarrow \mu = 0.756$

Segment 2: $24.5^\circ \rightarrow \mu = 0.5$

Segment 3: 63.5° say $50^\circ \rightarrow \mu = 0.14$

Snow loads:

Segment 1: 0.68 kPa

Segment 2: 0.45 kPa

Segment 3: 0.127 kPa

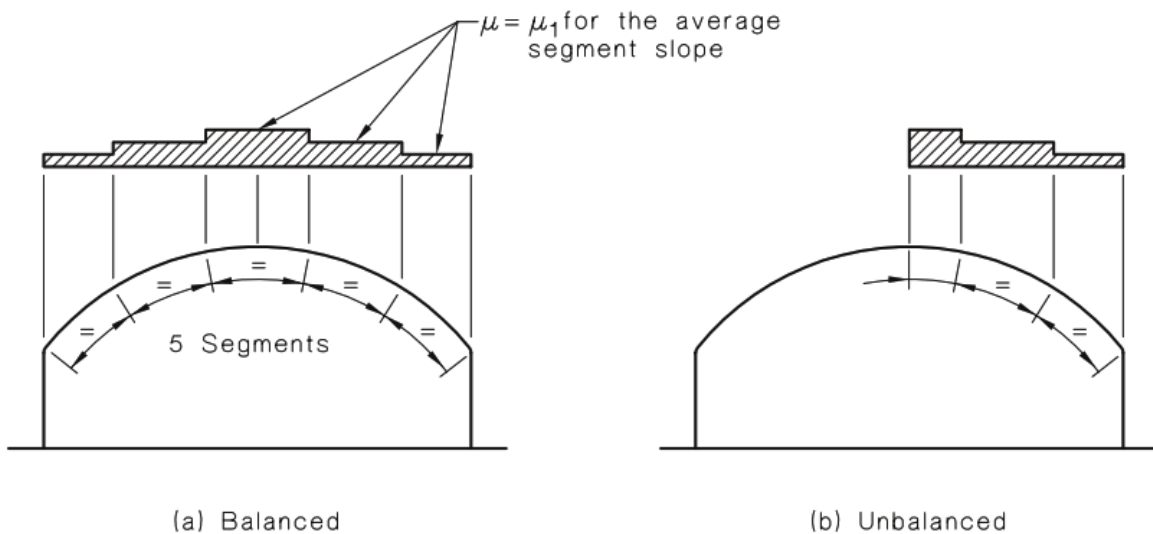
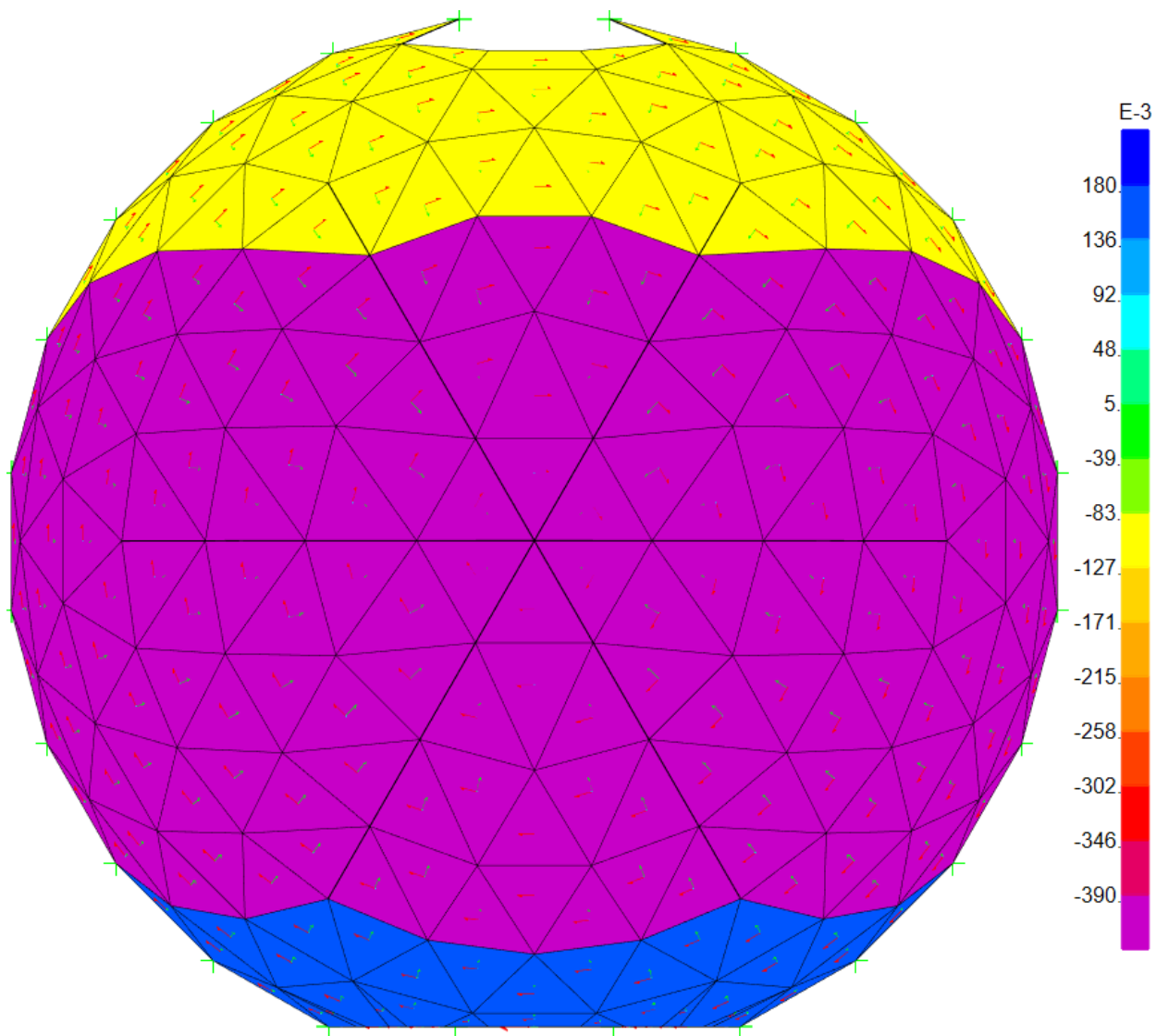


FIGURE 7.4 TYPES OF SNOW LOAD ON CURVED ROOFS (SUB-ALPINE)

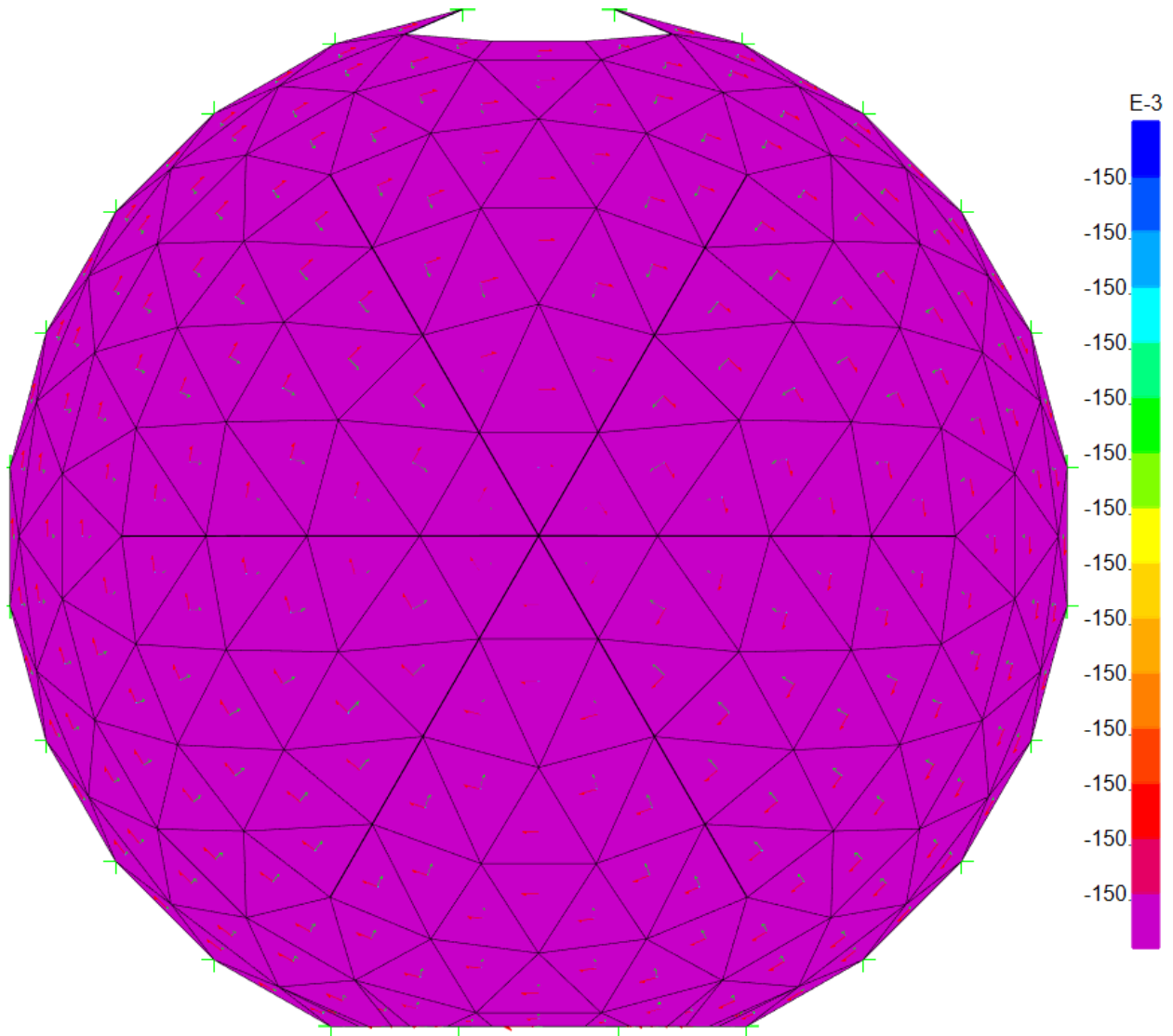
7 Load Diagrams

7.1 Wind Load

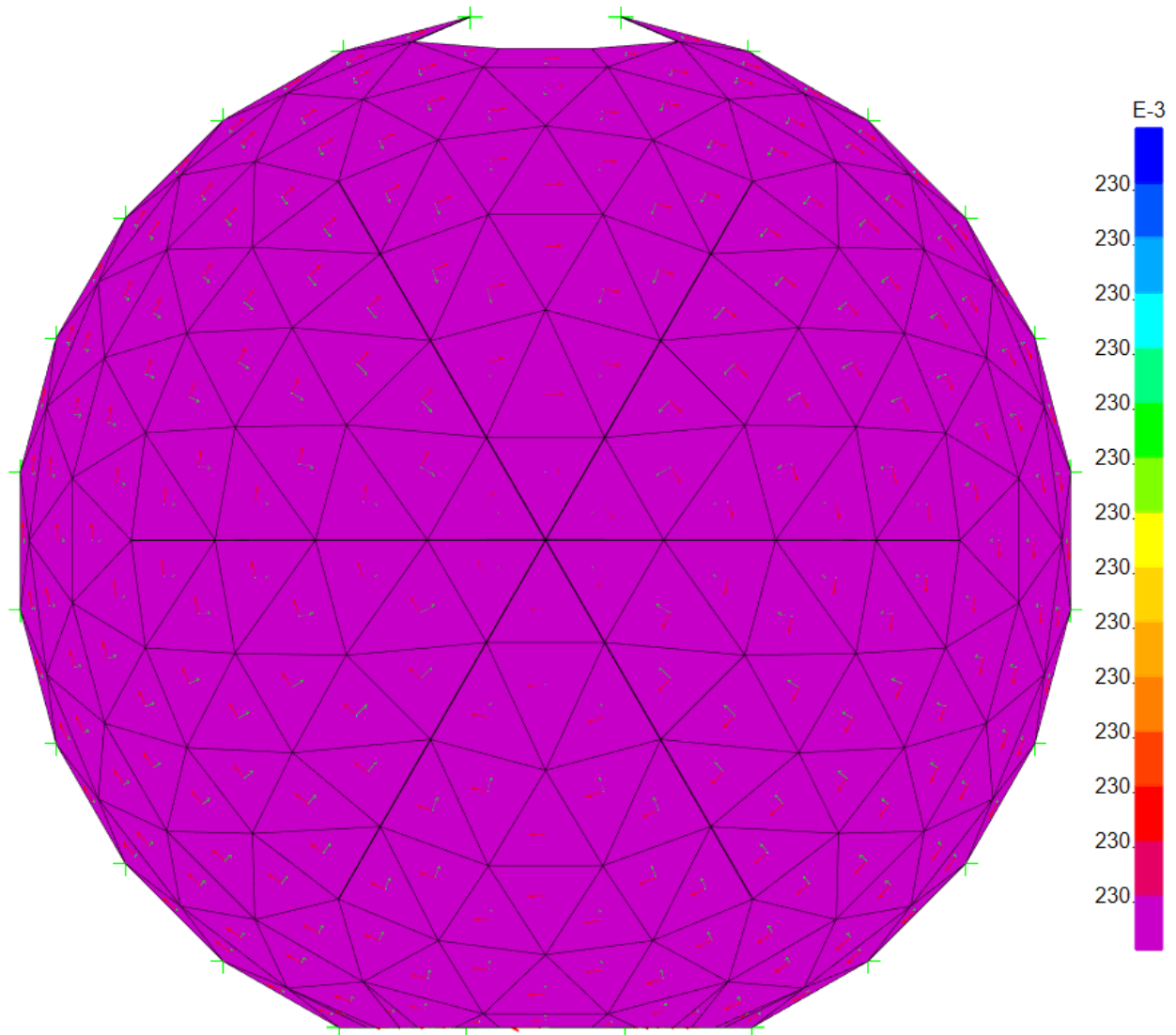
7.1.1 Wind Load Ultimate (W_u)



7.1.2 Wind Load Internal Pressure ($W_{i,pressure}$)

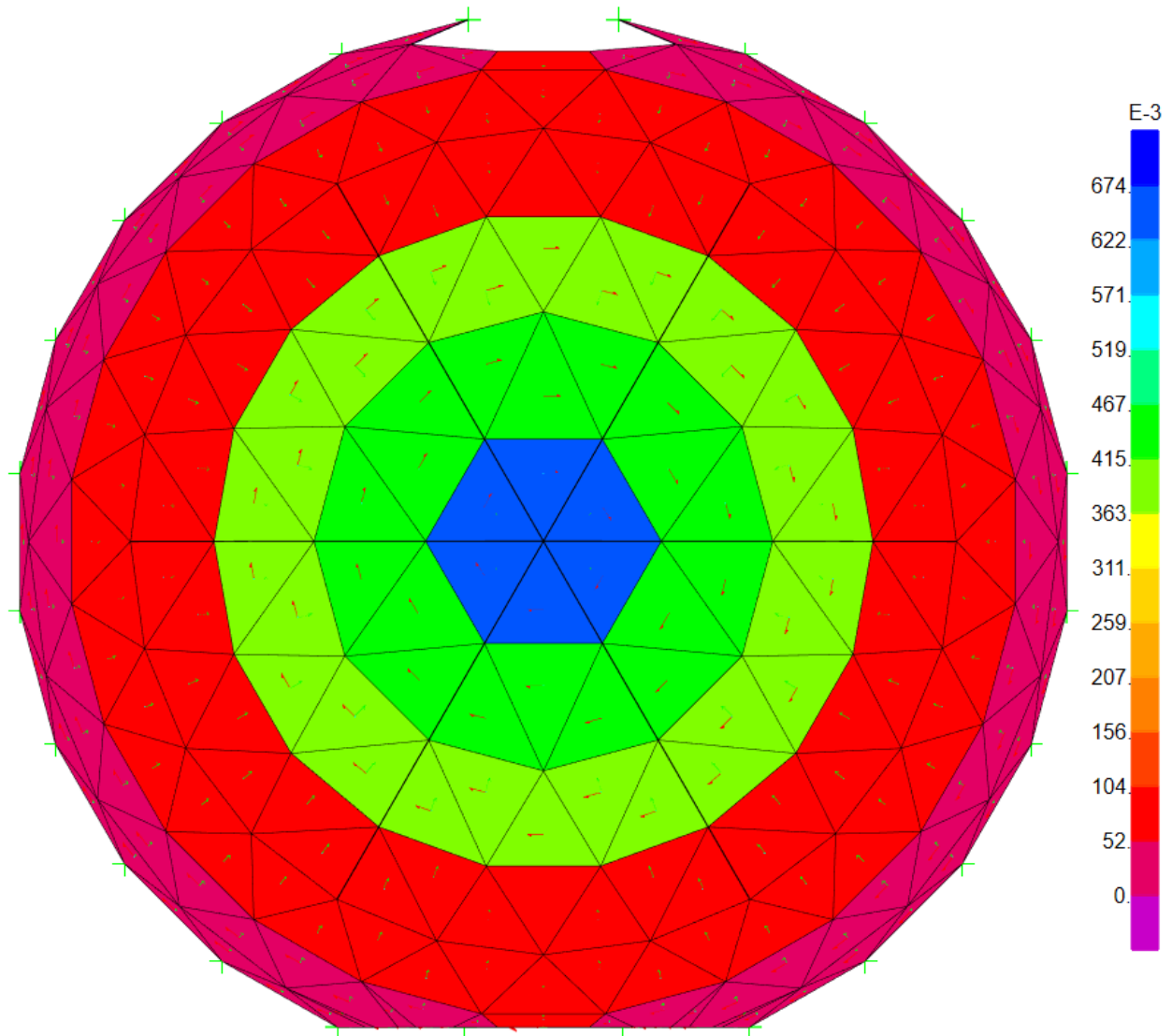


7.1.3 Wind Load Internal Suction ($W_{I,suction}$)

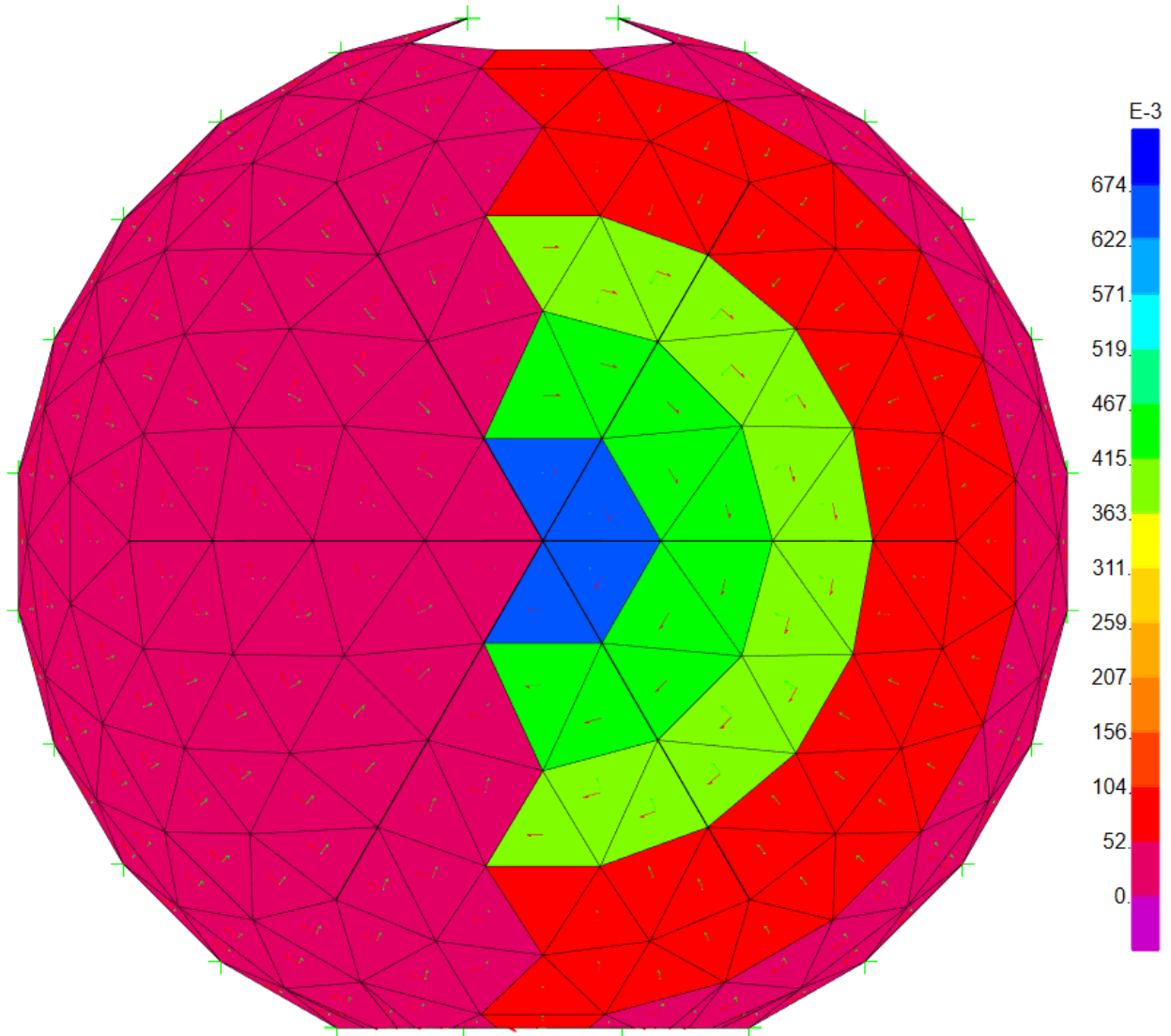


7.2 Snow Load

7.2.1 Snow Load (Case1)

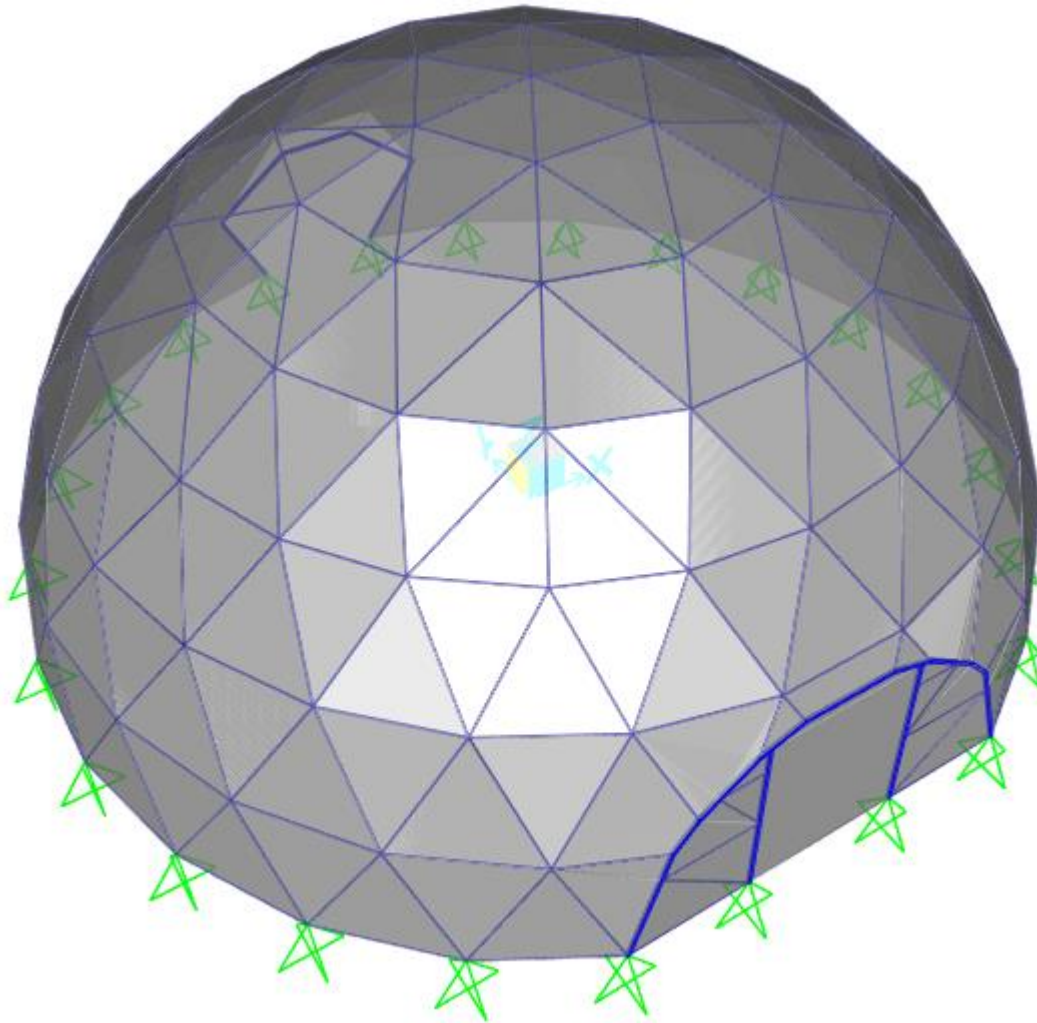


7.2.2 Snow Load (Case2)



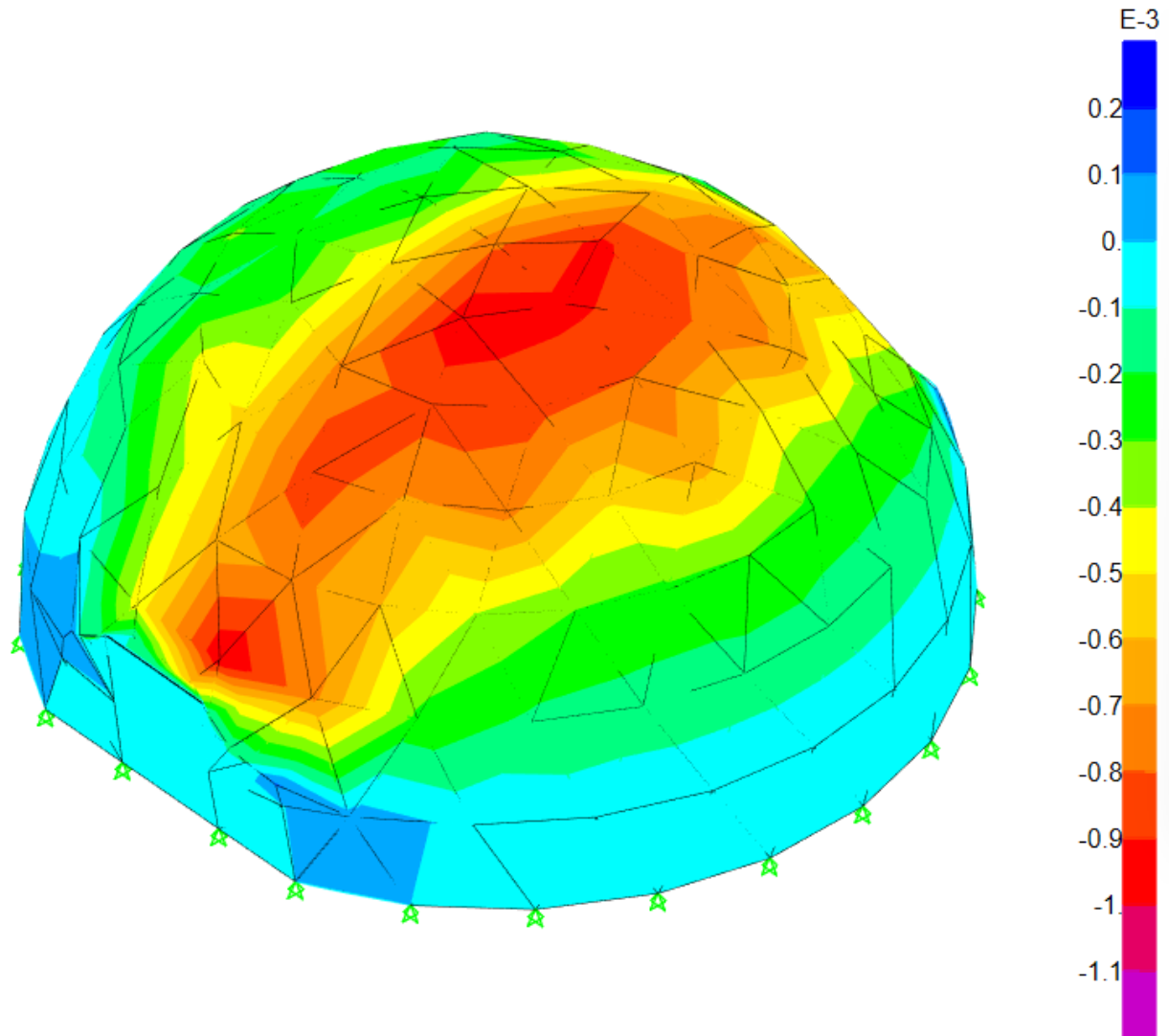
8 Analysis

8.1 3D model

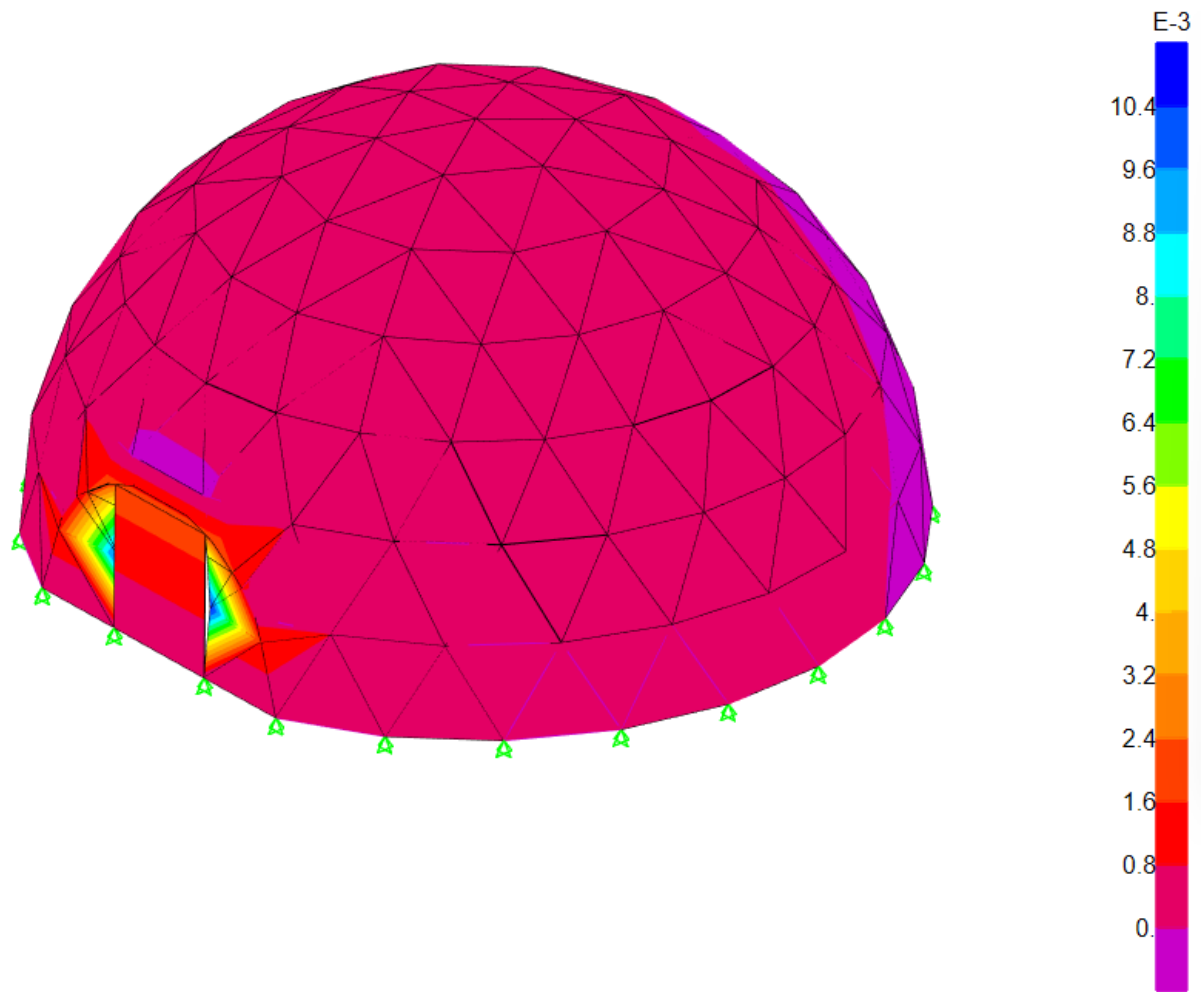


8.2 Results

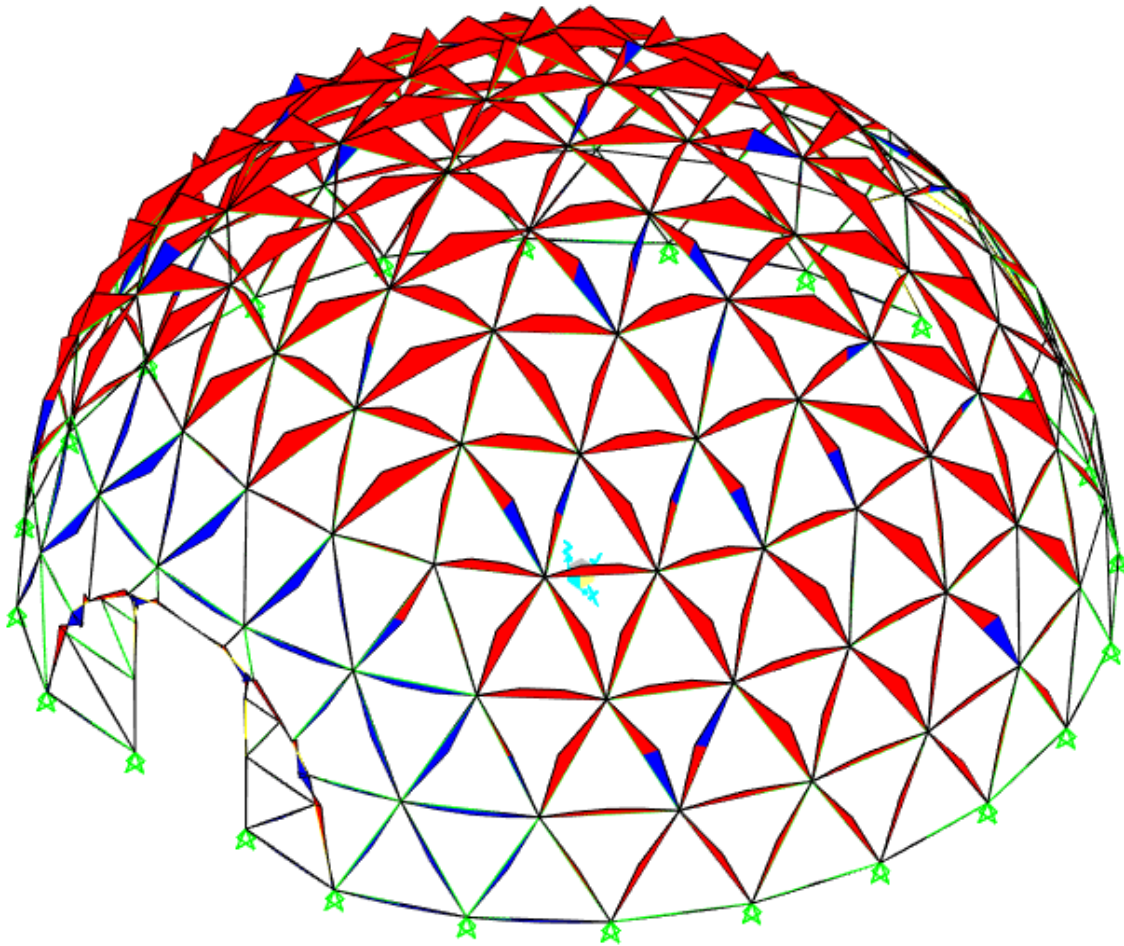
8.2.1 Maximum vertical deflection (serviceability)



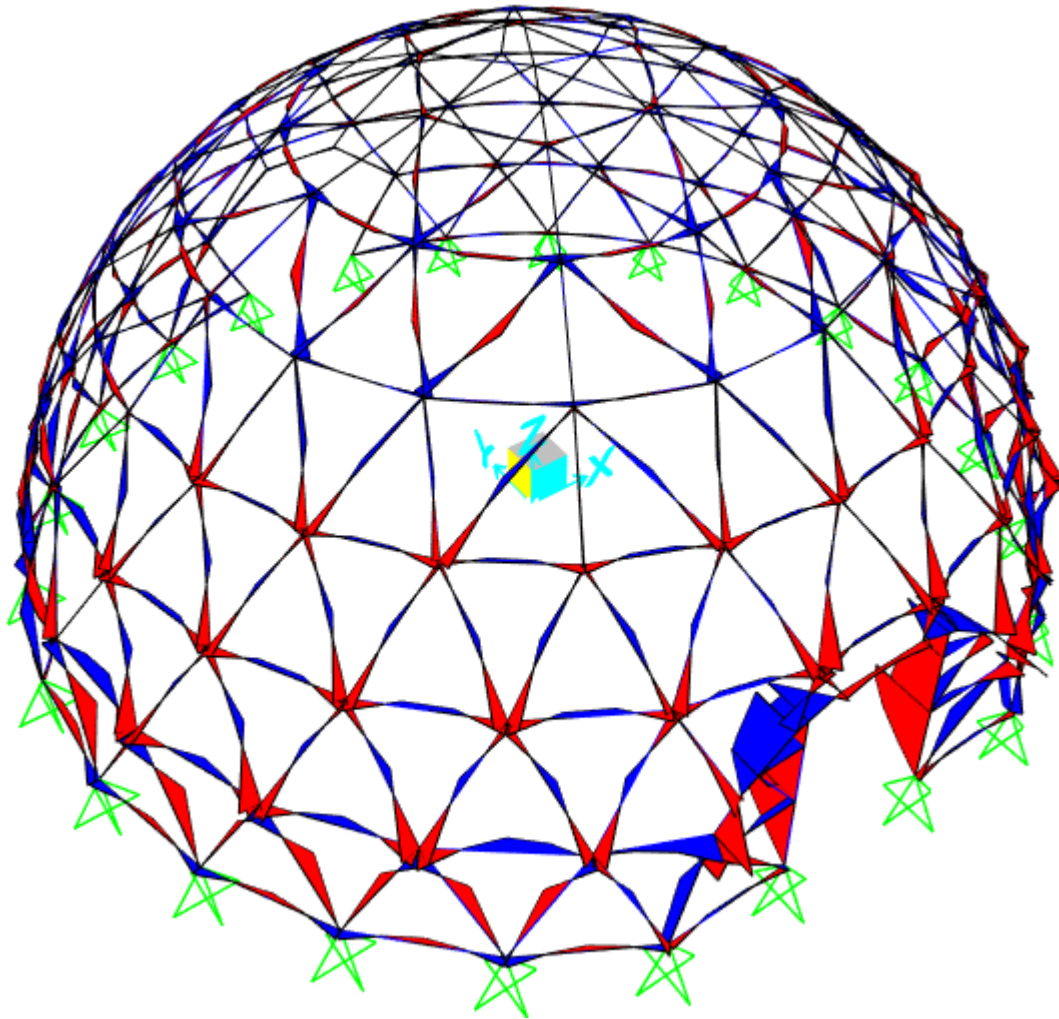
8.2.2 Maximum horizontal deflection (serviceability)



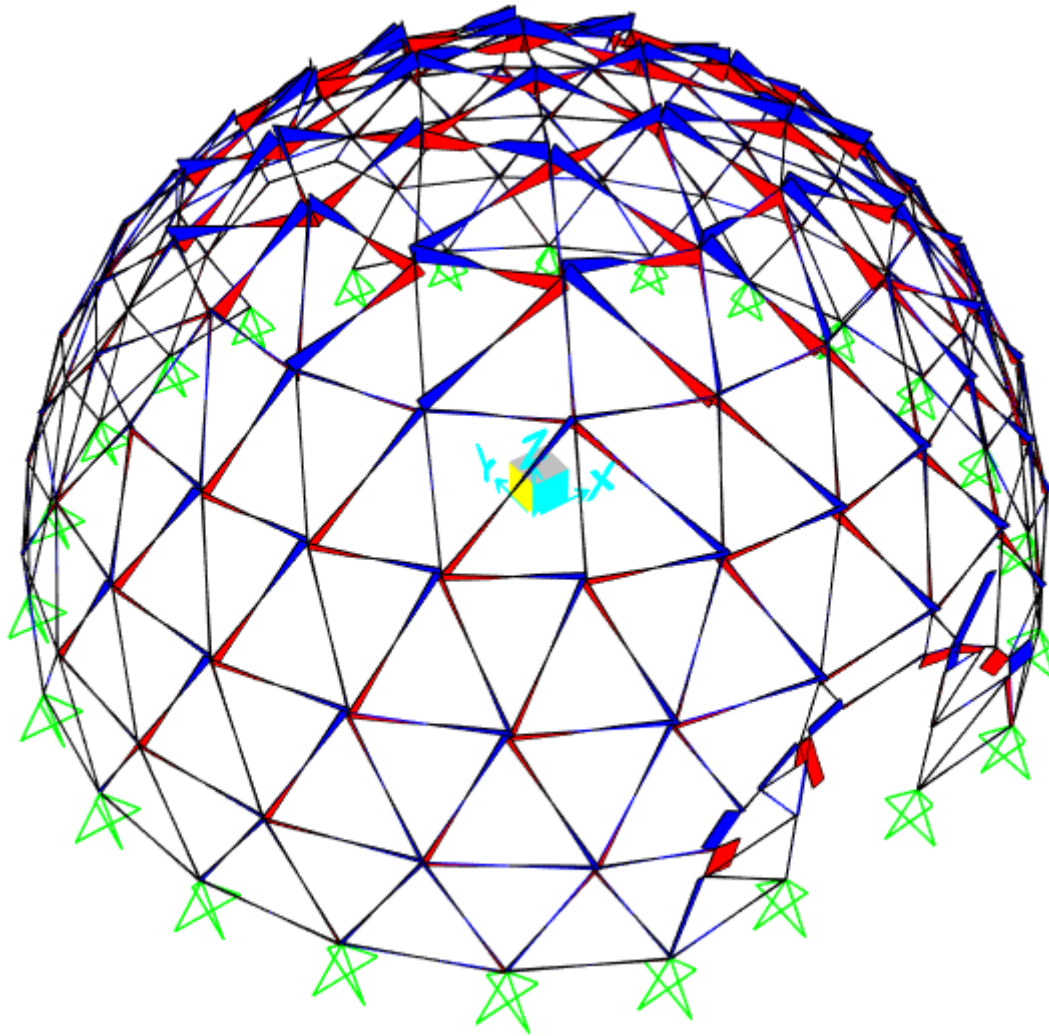
8.2.3 Maximum Bending Moment in Major Axis



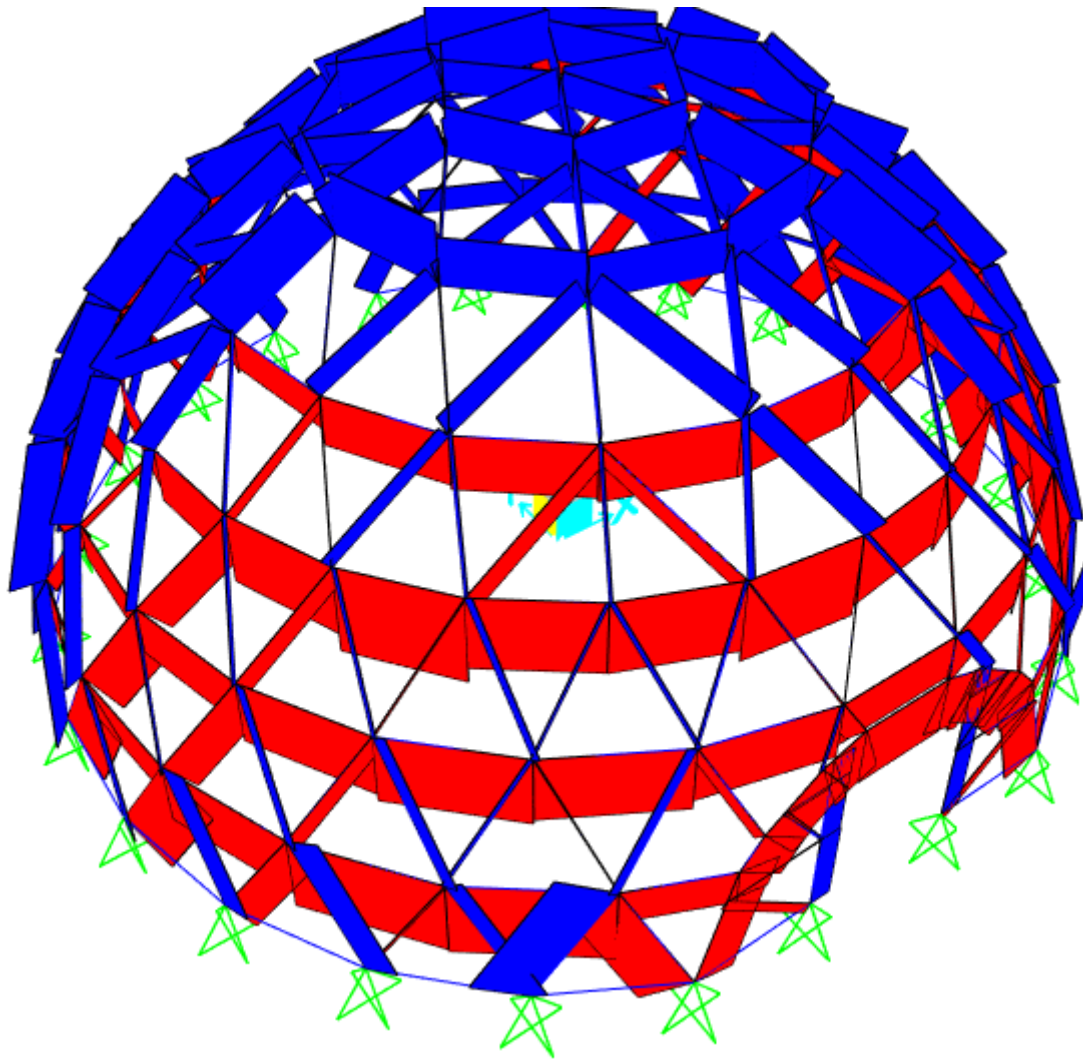
8.2.4 Maximum Bending Moment in Minor Axis



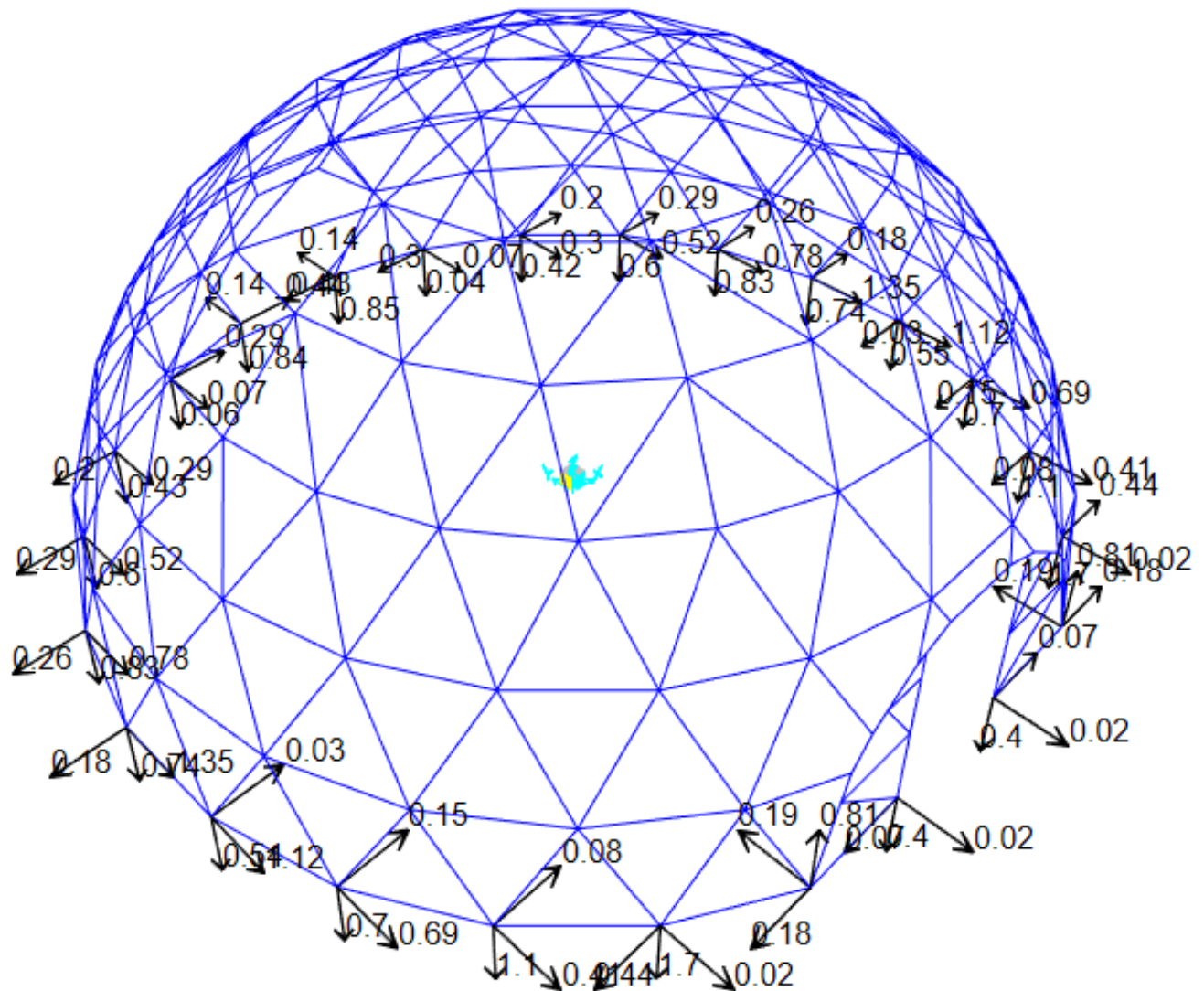
8.2.5 Maximum Shear



8.2.6 Maximum Axial Force



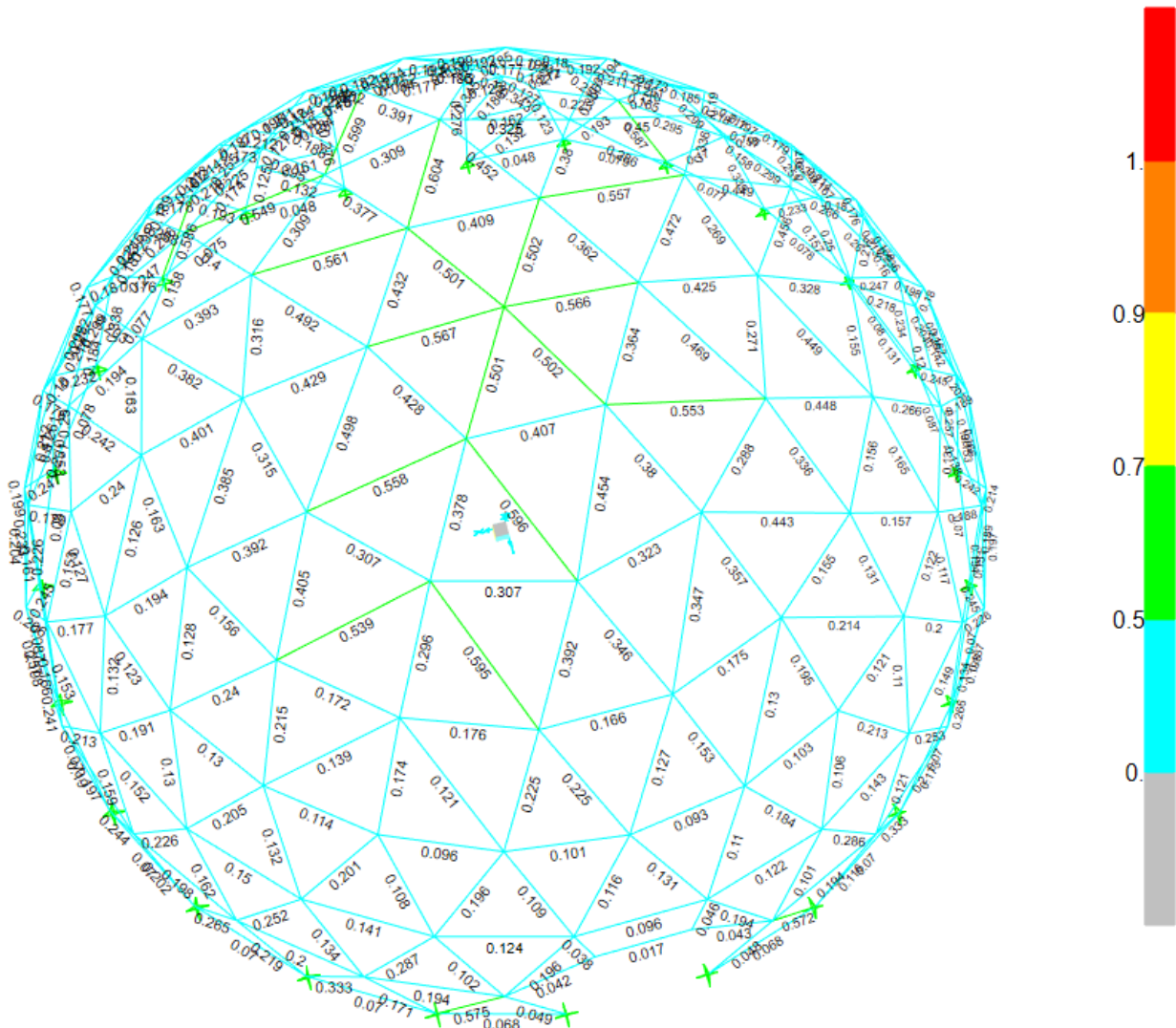
8.2.7 Maximum Reactions



Max. $F_x = 1.8 \text{ kN}$
 Max. $F_y = 1.75 \text{ kN}$
 Max. $F_z, \text{ Bearing} = 4.7 \text{ kN}$
 Max. $F_z, \text{ uplift} = 2.92 \text{ kN}$

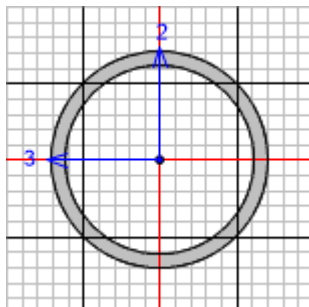
9 Steel Member Design

All members pass for the defined design wind actions. Refer to Appendix 'B' for section capacities and factor of safeties.



All members Pass

9.1 32x2 CHS



AS 4100-1998 STEEL SECTION CHECK (Summary for Combo and Station)
Units : KN, m, C

Frame : 363	X Mid: 1.001	Combo: COMB8	Design Type: Beam
Length: 1.335	Y Mid: 0.578	Shape: 32x2 CHS	Frame Type: Braced Frame
Loc : 0.445	Z Mid: 5.85	Class: Compact	Princpl Rot: 0. degrees

PhiB=0.9	PhiC=0.9	PhiTY=0.9	PhiTF=0.9	PhiS=0.9
A=1.885E-04	I33=2.130E-08	r33=0.011	Z33=1.331E-06	Av3=9.453E-05
J=4.260E-08	I22=2.130E-08	r22=0.011	Z22=1.331E-06	Av2=9.453E-05
E=210000000.	Fy=235000.	Ry=1.106	S33=1.803E-06	Iw=0.
RLLF=1.	Fu=390000.	SteelType=HR	S22=1.803E-06	

STRESS CHECK FORCES & MOMENTS (Combo COMB8)

Location	N*	M33*	M22*	V2*	V3*	T*
0.445	-1.85	0.066	-1.483E-04	-0.095	-4.919E-04	7.216E-05

PMM DEMAND/CAPACITY RATIO (8.3.4a)
D/C Ratio: 0.232 = 0.046 + 0.186 + 0. < 0.95 OK
= N*/(phi*Ns) + M33*/(phi*Ms33) + M22*/(phi*Ms22)

BASIC FACTORS

Buckling Mode	K Factor	L Factor	KL/r
Major Flexure	1.	1.	125.598
Minor Flexure	1.	1.	125.598
Major Braced	1.	1.	125.598
Minor Braced	1.	1.	125.598
LTB	1.4	1.	175.837

AXIAL FORCE & BIAXIAL MOMENT DESIGN (8.3.4a)

Factor	L	Braced	ke	Sway	ke	Delta_b	Delta_s	Cm	Betam
Major Bending	1.	1.	1.	1.	1.	1.081	1.	1.	-1.
Minor Bending	1.	1.	1.	1.	1.	1.	1.	0.285	0.788

LTB Factors	Lltb	Kt	Kl	Kr	Alpha_m	Alpha_s
	1.	1.	1.4	1.	1.166	1.001

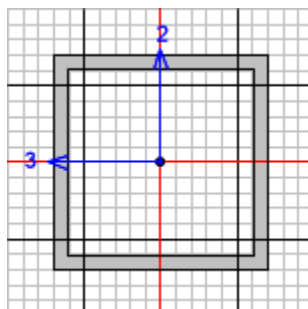
Axial Factors	Steel Type	Kf	Kt	Alpha_a	Alpha_b	Alpha_c
	HR	1.	1.	15.143	-1.	0.498

Element	Lambda_e	Lambda_ep	Lambda_ey	Lambda_ew	Compactness
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Bending	Any	15.04	50.	120.	1.000E+14	Compact
Axial	Any	15.04		82.		Compact
Effective Pro	ZeMajor	ZeMinor	de	Aeff		
	1.803E-06	1.803E-06	0.032	1.885E-04		
Major Moment	M*	Ms	Mr	Mi	Nc	
	0.071	0.424	0.404	0.384	22.056	
Minor Moment	-1.483E-04	0.424	0.404	0.384	22.056	
Major Moment	Mo,cr	Mb	Mo	Mc	Mt	
	6.594	0.424	0.384	0.384	0.384	
Axial	N*	Ns	Nc	Nt	Noz	
	-1.85	44.296	22.056	44.296	15224.641	
SHEAR CHECK						
Major Shear	V*	Vv	Stress	Status		
	Force	Capacity	Ratio	Check		
	0.095	14.352	0.007	OK		
Minor Shear	4.919E-04	14.352	3.427E-05	OK		

9.2 30x2 SHS



AS 4100-1998 STEEL SECTION CHECK (Summary for Combo and Station)
Units : KN, m, C

Frame : 14	X Mid: 2.129	Combo: COMB8	Design Type: Brace
Length: 1.4	Y Mid: -5.51	Shape: 30x2 SHS	Frame Type: Braced Frame
Loc : 0.	Z Mid: 0.668	Class: Compact	Princpl Rot: 0. degrees

PhiB=0.9 PhiC=0.9 PhiTY=0.9 PhiTF=0.9 PhiS=0.9

A=2.240E-04	I33=2.942E-08	r33=0.011	Z33=1.961E-06	Av3=1.200E-04
J=4.390E-08	I22=2.942E-08	r22=0.011	Z22=1.961E-06	Av2=1.200E-04
E=210000000.	Fy=235000.	Ry=1.106	S33=2.356E-06	Iw=0.
RLLF=1.	Fu=390000.	SteelType=HR	S22=2.356E-06	

STRESS CHECK FORCES & MOMENTS (Combo COMB8)

Location	N*	M33*	M22*	V2*	V3*	T*
0.	-5.354E-05	-0.062	0.041	-0.238	0.045	-8.282E-04

PMM DEMAND/CAPACITY RATIO (8.4.4.1)

D/C Ratio: 0.125 = 0.125 < 0.95 OK
= M33*/(phi*Mo33)

BASIC FACTORS

Buckling Mode	K Factor	L Factor	KL/r
Major Flexure	1.	0.749	91.452
Minor Flexure	1.	1.	122.166
Major Braced	1.	0.749	91.452
Minor Braced	1.	1.	122.166
LTB	1.4	1.	171.033

AXIAL FORCE & BIAXIAL MOMENT DESIGN (8.4.4.1)

Factor	L	Braced	ke	Sway	ke	Delta_b	Delta_s	Cm	Betam
Major Bending	0.749	1.	1.	1.	1.	1.	1.	0.376	0.561
Minor Bending	1.	1.	1.	1.	1.	1.	1.	0.2	1.

LTB Factors	Lltb	Kt	Kl	Kr	Alpha_m	Alpha_s
	1.	1.	1.4	1.	2.5	0.996

Axial Factors	Steel Type	Kf	Kt	Alpha_a	Alpha_b	Alpha_c
	HR	1.	1.	15.447	-1.	0.521

Slenderness	Lambda_e	Lambda_ep	Lambda_ey	Lambda_ew	Lambda_e/ey	Compactness
Major/Flange	12.604	30.	45.	180.	0.28	Compact
/Web	12.604	82.	115.	180.	0.11	Compact
Minor/Flange	12.604	82.	115.	180.	0.11	Compact



/Web	12.604	30.	45.	180.	0.28	Compact
Axial/Flange	12.604		45.		0.28	Compact
/Web	12.604		45.		0.28	Compact
Effective Pro	ZeMajor 2.356E-06	ZeMinor 2.356E-06	b-be 0.	d-de 0.	Aeff 2.240E-04	
Major Moment	M* -0.062	Ms 0.554	Mr 0.554	Mi 0.554	Nc 39.314	
Minor Moment	0.041	0.554	0.554	0.554	27.432	
Major Moment	Mo,cr 7.502	Mb 0.554	Mo 0.554	Mc 0.554	Mt 0.554	
Axial	N* -5.354E-05	Ns 52.64	Nc 27.432	Nt 52.64	Noz 13500.351	
SHEAR CHECK						
Major Shear	V* Force 0.238	Vv Capacity 15.228	Stress Ratio 0.016	Status Check OK		
Minor Shear	0.045	15.228	0.003	OK		



10 Pegging Design



Project: 12m Dome

Jon no. 22-211-1

Date: 4/05/2022

Name	Value	Unit	Notes
<u>minimum embedment depth for lateral bearing:</u>			
Max. Horizontal Force	1.75	kN	
Max. Vertical Force	2.92	kN	
Number of Pegs	3		
Horizontal Load per peg	0.6	kN	
Vertical Load per peg	1.0	kN	
Sticking out of Ground	0	m	
S (bearing capacity)	150	kPa	To be confirmed by Geotechnical engineer
φ	0.02	m	
H	194	mm	
M	0.00	kNm	
γ	19	kN/m ³	To be confirmed by Geotechnical engineer
min required Embedment:	194	mm	
F.S	6.17		
	OK		
<u>Bending:</u>			
Profile	φ 20mm Peg		
Fy	350	mPa	
Ze	785.4	mm ³	
phi	0.9		
phi Ms	0.25	kNm	
	OK		
<u>Pull out Checking:</u>			
Clay:			
Cu	25	kPa	To be confirmed by Geotechnical engineer



α (reduction factor)	1	
Provided Embedment	1200	mm
L/d	60	
Rs	0.96	
Perimeter	63	mm
Total Surface Area	0.075	m ²
min required Embedment:	0.65	m
F.S	1.85	
	OK	
Coefficient of Friction	0.6	
Equivalent Ballast	0.29	tonne
Reference: Foundations of Structures - Dunham, Mc Graw-Hill		

11 Summary and Recommendations

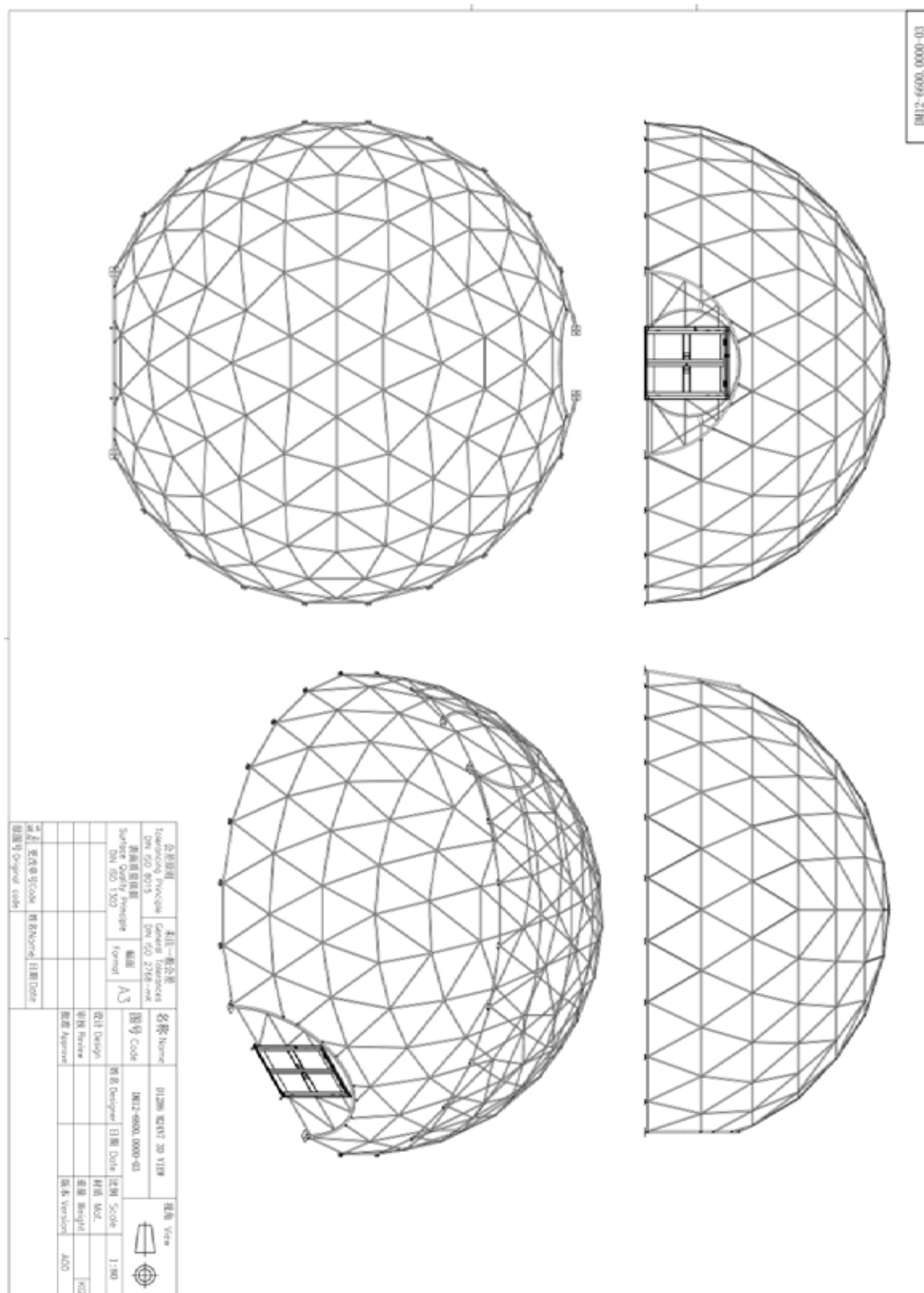
- The 12m Dome Structure as specified is capable of withstanding 3s gust wind speed up to **140km/hr** in region A, TC2.
- The dome structure is required to be dismantled for forecast winds in excess of **140km/hr**.
- The dome structure is designed to withstand snow loads of sub-alpine region (Orange, NSW) with maximum ground snow (Sg) 0.9kPa.
- For uplift due to 140km/hr, 3 kN (300kg) holding down weight/per support is required. (24 anchor points in total). Alternatively, pegging system described in Cl. 10 can be used.
- Design of fabric is by others.

Yours faithfully,

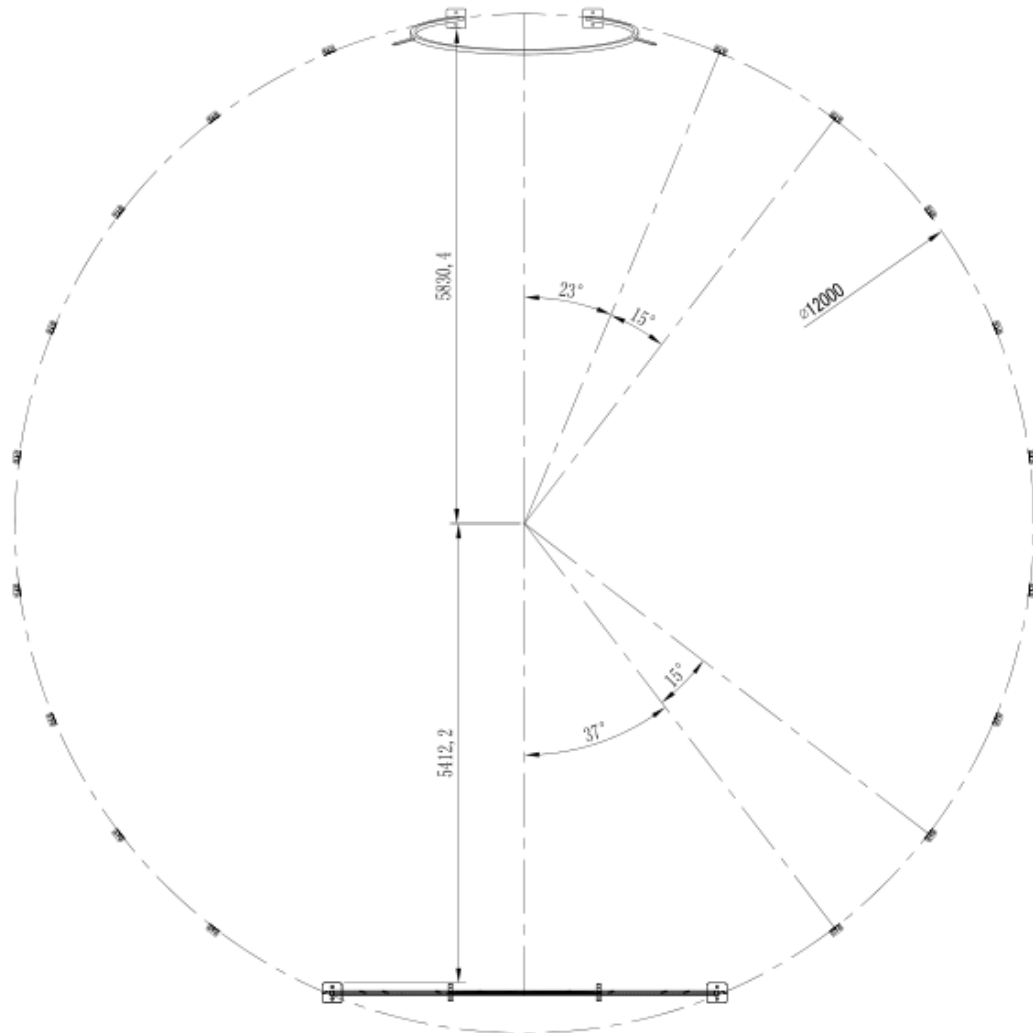
Prime Consulting Engineers Pty. Ltd.

Kevin Zia, BEng, Meng, MIEAust, CPENG NER

12 Appendix A – Detail Drawings



DM12-6600.0000-02



公差原则 Tolerancing Principle DIN ISO 8015		未注一般公差 General Tolerances DIN ISO 2768-mK		名称 Name		D12H6 M24N7 ORIENTATION PLAN		视角 View			
表面质量依据 Surface Quality Principle DIN ISO 1302		幅面 Format		A4		图号 Code		DM12-6600.0000-02			
						姓名 Designer	日期 Date	比例 Scale	1:1		
						设计 Design		材质 Mat.	Q235B		
						审核 Review		重量 Weight	*	KG	
						批准 Approve		版本 Version	A00		
更改单号 Code		姓名 Name		日期 Date							
原图号 Original code											

